



Research paper

Thermal stability and fracture patterns of a recently synthesized monolayer fullerene network: A reactive molecular dynamics study

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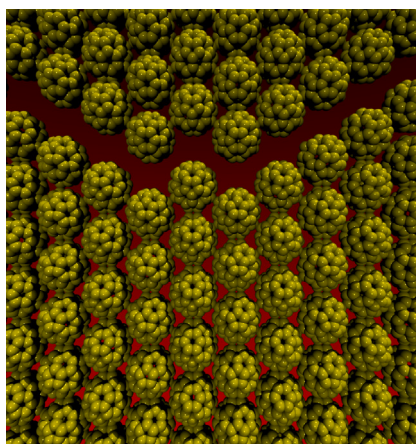
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HIGHLIGHTS

- qHPC60 and qTPC60 have melting points about 3900K.
- qHPC60 and qTPC60 have anisotropic mechanical properties.
- qHPC60 and qTPC60 have elastic modulus of 175.9 and 100.7 GPa, respectively.

GRAPHICAL ABSTRACT



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ABSTRACT

New monolayer 2D carbon structures, namely qHPC₆₀ and qTPC₆₀, were recently synthesized by covalently bonding C₆₀ polymers. Here, we carried out Reactive (ReaxFF) molecular dynamics simulations to study the thermodynamic stability and fracture patterns of qHPC₆₀ and qTPC₆₀. Our results showed that these structures present similar thermal stability, with sublimation points of 3898K and 3965K, respectively. qHPC₆₀ and qTPC₆₀ undergo an abrupt structural transition becoming totally fractured after a critical strain threshold. The crack propagation is linear (non-linear) for qHPC₆₀ (qTPC₆₀). The estimated elastic modulus for qHPC₆₀ and qTPC₆₀ are 175.9 GPa and 100.7 GPa, respectively.

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1. Introduction

Since the discovery of graphene [1], 2D carbon materials have been widely studied to develop new optoelectronic applications [2]. Their controllable synthesis can yield different structures with distinct physical and chemical properties [3,4]. Due to this reason, the large variety of 2D carbon allotropes proposed so far [5–14] have proven to be suitable for flat electronics, although only a few structures has been experimentally realized.

Recently, new 2D carbon allotropes were synthesized: the monolayer amorphous carbon (MAC) [11] and the 2D biphenylene network (BPN) [12]. MAC is made of randomly distributed five, six, seven, and eight atom rings. BPN consists of a periodic lattice composed of fused rings containing four, six, and eight carbon atoms. Similar to graphene, MAC and BPN present a zero semi-metal bandgap, which is a serious drawback to their usage in some optoelectronic applications [15].

Very recently, 2D carbon materials with a semiconducting bandgap of about 1.6 eV – namely monolayer quasi-hexagonal-phase fullerene (qHPC₆₀) and monolayer quasi-tetragonal-phase fullerene (qTPC₆₀) – were experimentally realized overcoming the problem of a null bandgap shown by other 2D carbon-based materials [16]. It was reported that qHPC₆₀ and qTPC₆₀ show excellent environmental and thermal stabilities. The Raman spectra and optical images remain unchanged after heating, indicating that the polymeric C₆₀ frameworks do not decompose up to 600 K. qHPC₆₀ and qTPC₆₀ exhibit high crystallinity and unique topological structure [16]. In this sense, a detailed description of their structural integrity with a focus on thermodynamic stability and stress resilience can pave the way for its applications.

In the present work, we investigated the thermodynamic stability and stress resilience of qHPC₆₀ and qTPC₆₀. It was observed that these materials present a well-defined (linear) elastic region when subjected to uniaxial strain. qHPC₆₀ and qTPC₆₀ undergo an abrupt structural transition to a totally fractured form after a critical strain threshold. The crack propagation is linear for qHPC₆₀ and non-linear for qTPC₆₀, respectively. Heating ramp protocol simulations revealed that they are thermally stable up to 3898 K and 3965 K, respectively.

2. Methodology

We carried out fully-atomistic MD simulations with the reactive force field ReaxFF (by employing the parameter set for C/H/O [17, 18]), as implemented in LAMMPS [19]. A reactive potential is needed (it allows the formation and breaking of chemical bonds during the dynamics) for the fracture dynamics investigation. Fig. 1 illustrates the qHPC₆₀ and qTPC₆₀ structural models (supercells) used in the MD simulations. Both structures have dimensions of 100 × 100 Å² with periodic boundary conditions and are composed of 8640 atoms. The length of the simulation box along the z-direction is 200 Å.

The equations of motion were numerically integrated using the velocity-Verlet algorithm, with a time-step of 0.2 fs. The uniaxial tensile strain was applied along the periodic *x* and *y* directions, for an engineering strain rate of 1.0 × 10^{−6} fs^{−1}. Before their heating and stretching, the structures were equilibrated using an NPT ensemble at a constant temperature of 300 K and null pressures using a Nosé–Hoover thermostat [20] during 200 ps.

To obtain the mechanical properties and fracture patterns, the qHPC₆₀ and qTPC₆₀ structures were continuously stretched up to their complete structural failure (fracture) by applying a maximum strain of 50%. The tensile stretching simulations were performed by increasing the *x* and *y* cell dimensions. Their thermal stability was investigated by heating up the structures from 300 K up to 10,000 K. The heating process is simulated by linearly increasing the temperature during 1 ns in an NVT ensemble. The MD snapshots and trajectories were obtained using the visualization and analysis software VMD [21].

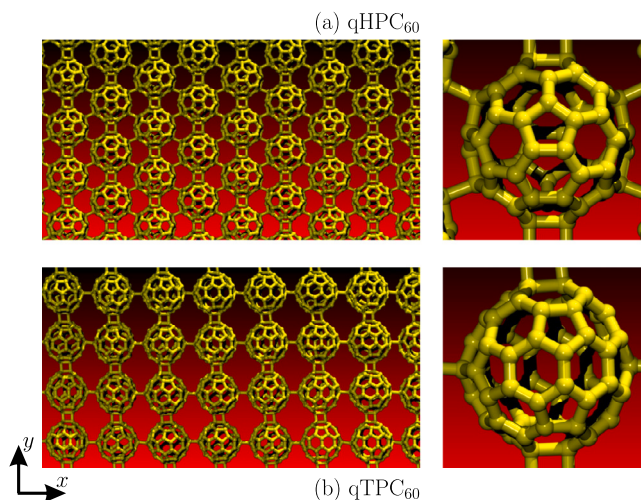


Fig. 1. Schematic representation of: (a) qHPC₆₀ and (b) qTPC₆₀ lattice structures. The right panels illustrate the corresponding unit cells.

3. Results

We begin our discussion by analyzing the qHPC₆₀ and qTPC₆₀ thermodynamic stability. The melting processes occur within the heating ramp simulations, as mentioned above. Fig. 3 illustrates the total energy (green) and heat capacity (*C_V*, in yellow) as a function of temperature for the melting process of qHPC₆₀ (Fig. 2(a)) and qTPC₆₀ (Fig. 2(b)). As a general trend, we can see that the total energy increases quasi-linearly with the temperature showing three different slopes: between 300 K–3500 K, 3500 K–4000 K, and 4000 K–10,000 K.

qHPC₆₀ and qTPC₆₀ maintain their structural integrity in the first stage of the heating process, defined by temperatures up to 3500 K. After this critical value, the thermal vibrations impose substantial changes in their morphologies, and the melting process occurs in the second stage of the heating process (for temperatures ranging from 3500 K up to 4500 K). The melting point is defined by the most pronounced peak in the *C_V* curves. In this sense, the peak in the heat capacity curve indicates the similar melting points at 3898 K (see Fig. 2(a)) and 3965 K (see Fig. 2(b)) for qHPC₆₀ and qTPC₆₀, respectively.

The third stage of the heating process (between 4000 K–10,000 K) in Figs. 2(a) and 2(b) characterizes the continuous heating of the systems. The abrupt change in the slope for the total energy curves defines a phase transition from a solid to a gas-like phase (sublimation) of the carbon atoms. The melting points obtained here for qHPC₆₀ and qTPC₆₀ are comparable to those for the monolayer graphene (4095 K) [22], MAC (3626 K) [23], and BPN (4024 K) [24].

We further explored the thermodynamic stability of qHPC₆₀ and qTPC₆₀ by analyzing the representative MD snapshots for the heating ramp simulations, with temperatures varying from 300 K up to 4000 K, as shown in Fig. 3. Figs. 2(a) and 2(e) illustrate the lattice structure for qHPC₆₀ and qTPC₆₀ at 0 K, respectively. In Figs. 2(b–c) and 2(f–g), we can note the melting process of these structures occurs differently. For the qHPC₆₀, the C₆₀ units are fragmented into several linear atomic chains (LACs) at 1600 K, while the qTPC₆₀ tends to fragment into separated C₆₀ units at 1200 K.

The complete atomization of the structures occurs at the related melting points, as shown in Figs. 2(d) and 2(h) for qHPC₆₀ and qTPC₆₀, respectively. Importantly, the different mechanisms observed in the melting processes are strictly related to their topology. qHPC₆₀ presents eight covalent bonds connecting the next-neighboring C₆₀ units, whereas qTPC₆₀ presents only six. The higher number of covalent bonds in qHPC₆₀ favors the formation of LACs before the lattice atomization at 1000 K (see Fig. 2(b)). Conversely, the qTPC₆₀ lower

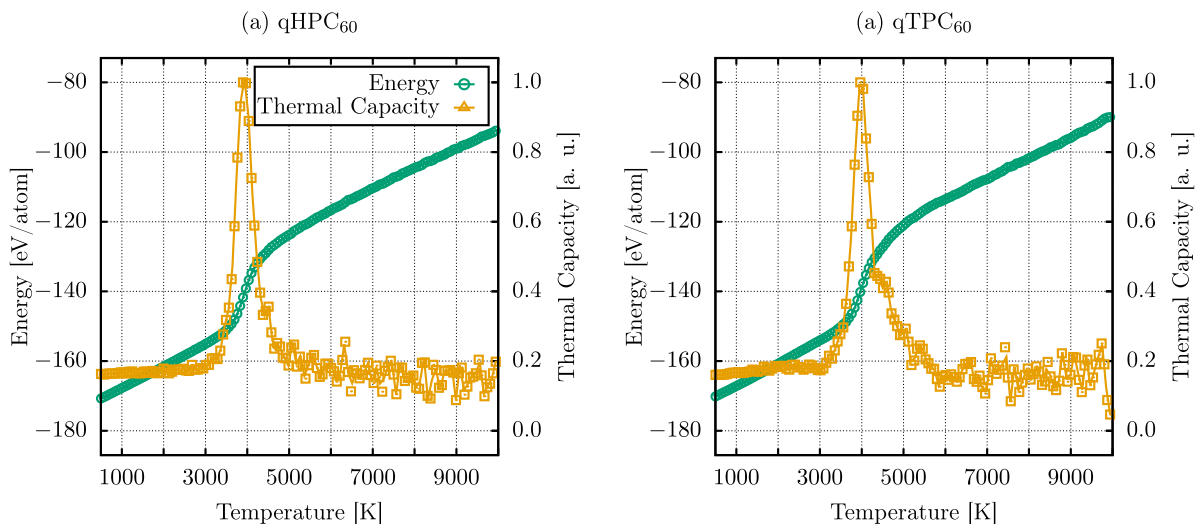


Fig. 2. Total energy and heat capacity (C_V) as a function of temperature for: (a) qHPC₆₀ and (b) qTPC₆₀ at 1 ns of the heating ramp simulations.

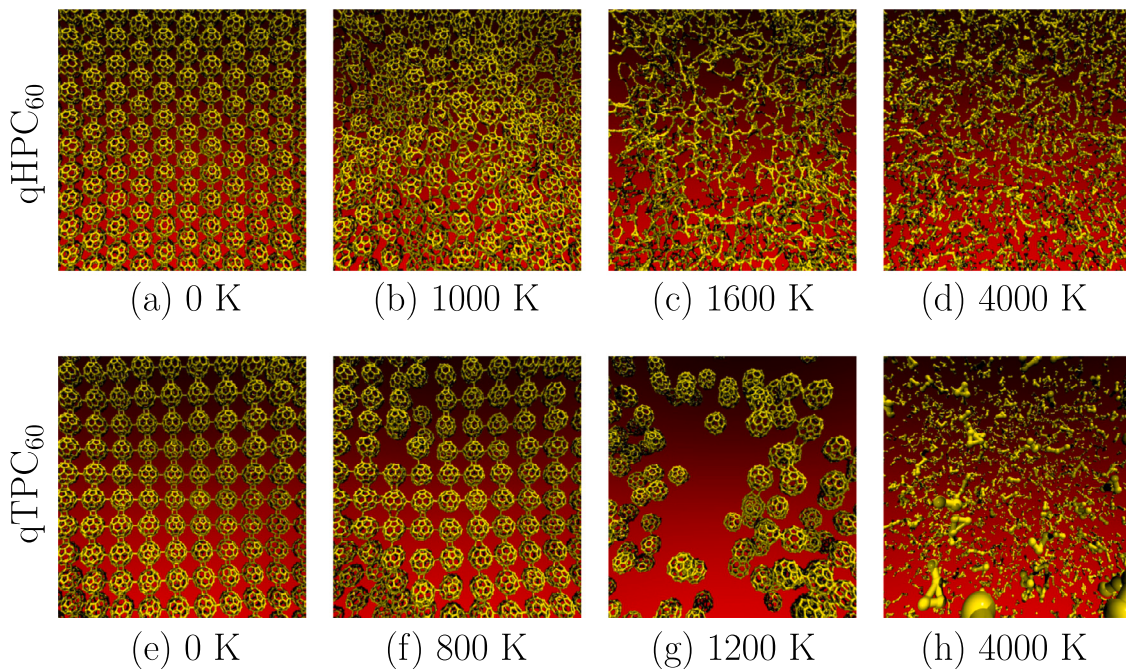


Fig. 3. Representative MD snapshots for the heating ramp simulations (melting process) for: qHPC₆₀ at (a) 0 K, (b) 1000 K, (c) 1600 K, and (d) 4000 K, and qTPC₆₀ at (e) 0 K, (f) 800 K, (g) 1200 K, and (h) 4000 K.

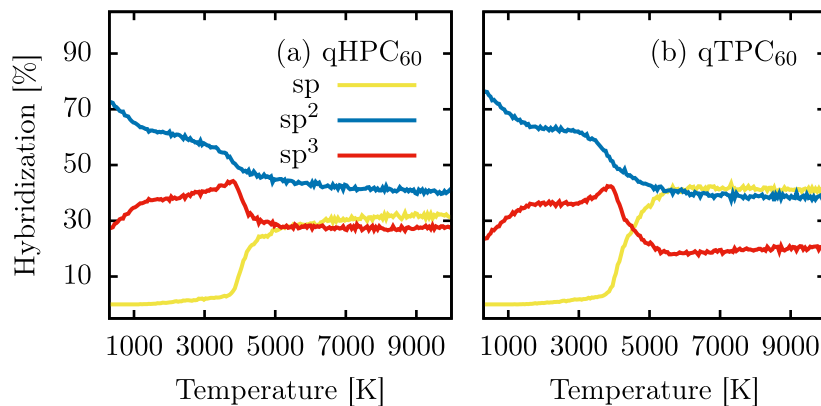


Fig. 4. Time evolution for the total number of different carbon-carbon bond types of (a) qHPC₆₀, and (b) qTPC₆₀, during their melting processes.

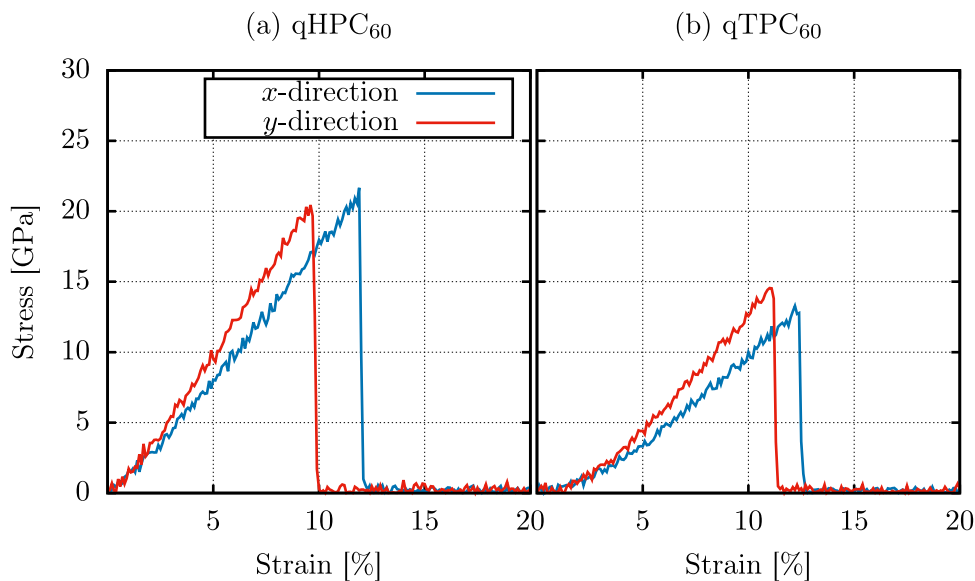


Fig. 5. Stress-strain curves for (a) qHPC₆₀ and (b) qTPC₆₀ as a function of the uniaxial applied strain in the (blue) x-direction and (red) y-direction.

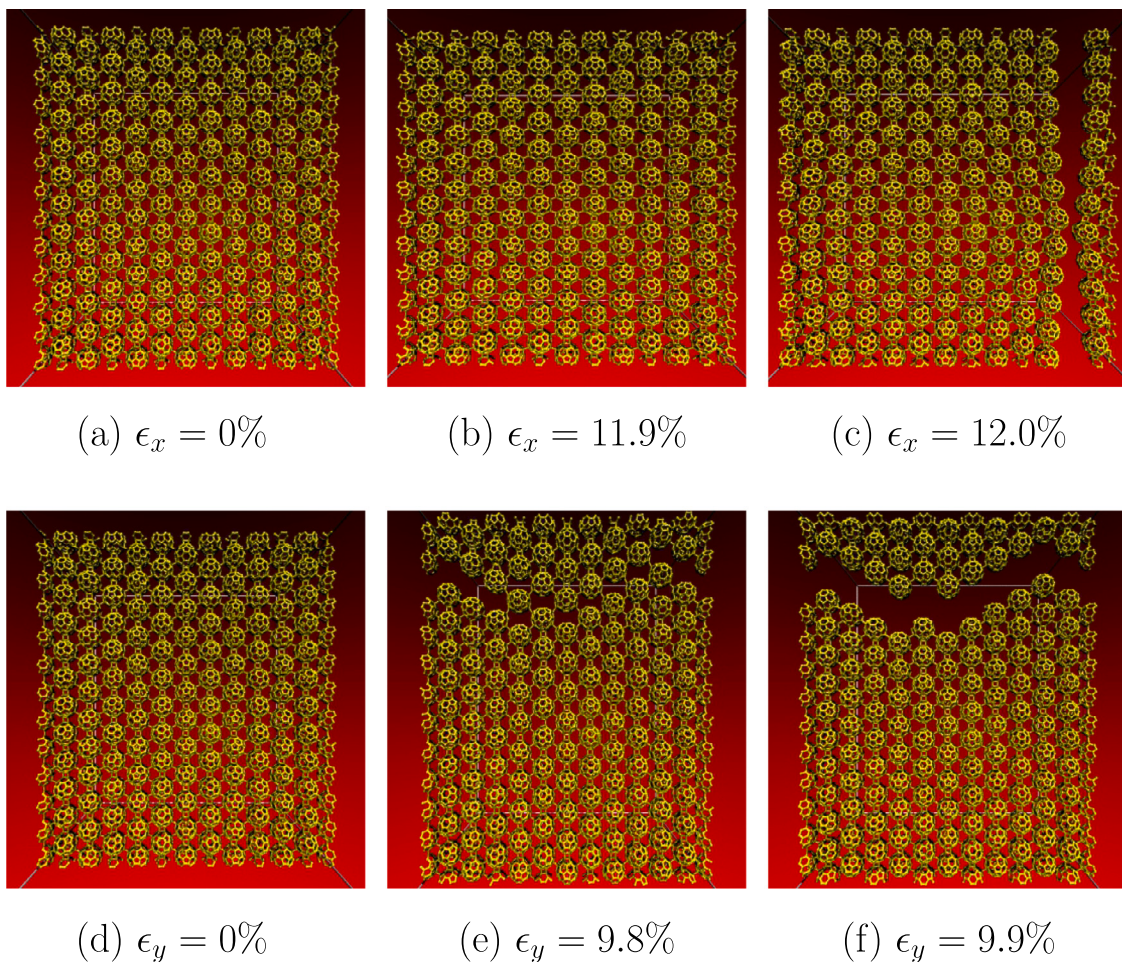


Fig. 6. Representative MD snapshots for the strain applied along the (a–c) x-direction (ϵ_x) and (d–f) y-direction (ϵ_y) for the qHPC₆₀ monolayer.

number of covalent bonds is responsible for its fragmentation into individual C₆₀ molecules at 800 K (see Fig. 2(f)).

To gain further insights into the melting processes of qHPC₆₀ and qTPC₆₀, Fig. 4 illustrates the time evolution for the total number of

different carbon–carbon bond types present in these C₆₀ crystals. There are two distinct stages to highlight in their melting processes: (I) the beginning of the crystal fragmentation into individual C₆₀ units, which occurs at 1000 K for qHPC₆₀ and 800 K for qTPC₆₀, respectively, and

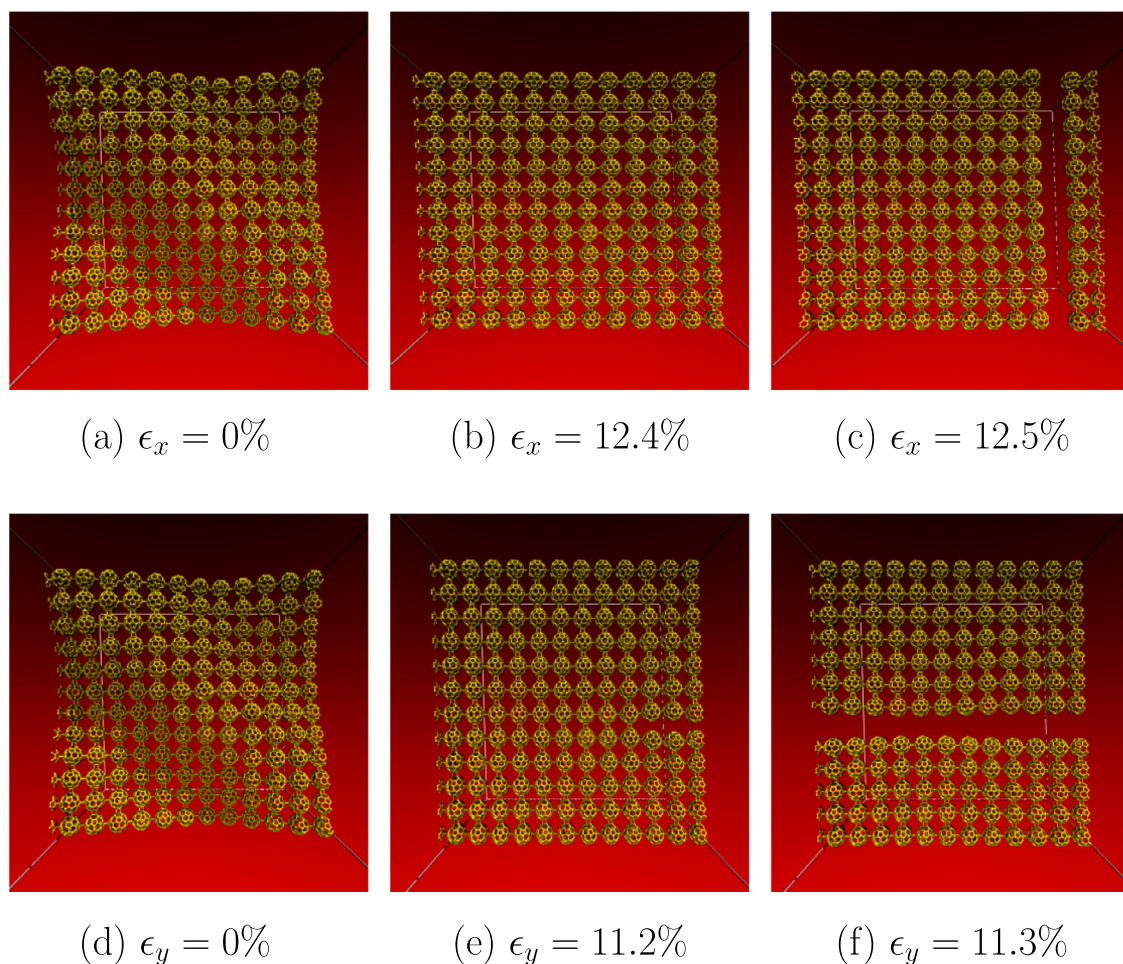


Fig. 7. Representative MD snapshots for the strain applied along the (a–c) x -direction (ϵ_x) and (d–f) y -direction (ϵ_y) for the qTPC₆₀ monolayer.

(II) the crystal atomization (defined as its melting point), which occurs at 3898 K for qHPC₆₀ and 3965 K for qTPC₆₀, respectively.

Figs. 4(a) and 4(b) show the total number of bonds (sp-like, sp²-like, and sp³-like C–C bonds) for the melting process of qHPC₆₀ and qTPC₆₀, respectively. Individual (bonded) C₆₀ molecules present both sp²- and sp³-like C–C bonds. In the qHPC₆₀ and qTPC₆₀ lattices, sp²-like bonds link the C₆₀ units. The sp-like bonds, in turn, are present in the linear atomic chains (LACS). We can see that the initial C₆₀ crystals only present sp²- and sp³-like C–C bonds and the hybridization percentage of sp²-like C–C bonds is zero, as expected. At temperatures lower than the melting points, the stage (I) of the melting process, the hybridization percentage of sp²-like C–C bonds is close to zero. This trend for the time evolution of the C–C bond types indicates that the C₆₀ units remain intact.

For temperatures higher than the qHPC₆₀ and qTPC₆₀ melting points, the stage (II) of the melting process, we can observe in Figs. 4(a) and 4(b) that the hybridization percentage of sp-like C–C bonds increases abruptly to about 30% and 40%, respectively. The hybridization percentage of sp²-like C–C bonds decreases smoothly until the end of the simulation, whereas the hybridization percentage of sp³-like bonds increases towards the melting temperature and then decreases for higher temperatures during the LACs formation.

The stress response as a function of the uniaxial applied strain is illustrated in Fig. 5. Figs. 5(a) and 5(b) show the stress–strain curves for the uniaxial tensile loading along the x -direction (blue) and y -direction (red) for qHPC₆₀ and qTPC₆₀, respectively. The first noticeable feature is that these structures have an anisotropic mechanical behavior, which is expected because of their structural anisotropy. qHPC₆₀ and qTPC₆₀

are more resilient to tension along the x -direction than for the y -one. The presence of a ring composed of four carbon atoms linking the C₆₀ units makes these structures less resilient to tension along the y -direction.

In Fig. 5, we can note that these materials present a well-defined (linear) elastic region when subjected to uniaxial strain. qHPC₆₀ and qTPC₆₀ undergo an abrupt transition from integrity to a fractured form after a critical strain of 9.6% (11.9%) along the x -direction (y -direction) and 12.2% (11.0%) along the x -direction (y -direction), respectively. The ultimate stress values for qHPC₆₀ and qTPC₆₀ are: 20.4 GPa (21.7 GPa) for the x -direction (y -direction) and 13.3 GPa (14.6 GPa) for the x -direction (y -direction), respectively. The ultimate stress is defined as the corresponding tensile stress for a critical strain. In our calculations, 1% of strain was used to estimate the following Young's modulus values for qHPC₆₀ and qTPC₆₀: 175.9 GPa (218.5 GPa) for the x -direction (y -direction) and 100.7 GPa (133.5 GPa) for the x -direction (y -direction), respectively. As mentioned above, qHPC₆₀ tends to be more resilient than qTPC₆₀ due to the higher number of covalent bonds connecting the next-neighboring C₆₀ units. These values are much lower than other 2D carbon-based structures and can be explained by the high structural stability of the C₆₀ units.

Finally, we discuss the fracture patterns of the qHPC₆₀ and qTPC₆₀ monolayer when subjected to uniaxial tensile loading. Figs. 6(a–c) and 6(d–f) show representative MD snapshots for the strain applied along the x -direction (ϵ_x) and y -direction (ϵ_y) for the qHPC₆₀ monolayer. Fig. 6(a) and 6(d) illustrate the monolayer configurations at $\epsilon_x = 0$ and $\epsilon_y = 0$, respectively. As can be inferred from Fig. 6(b), qHPC₆₀ preserves its topology as the strain increase up to $\epsilon_x = 11.9\%$. Immediately

after this critical strain value, the lattice breaks abruptly with fast and linear crack propagation along the opposite direction of the stretch (see Fig. 6(c)).

For the qHPC₆₀ stretching along the y -direction, a non-linear fast crack propagation is observed along the opposite direction of the stretch at 9.8% of strain, as shown in Fig. 6(e). The total fracture of qHPC₆₀ is achieved at 9.9% of strain (see Fig. 6(f)). The anisotropic trend for the fracture patterns of qHPC₆₀ is due to the different bond arrangements that connect the next-neighboring C₆₀ units along the directions of this 2D crystal. For the x -direction, four diagonal bonds connect a central unit to four neighboring units. On the other hand, along the y -direction, there are four parallel bonds linking only two neighboring units with a central one.

Figs. 7(a–c) and 7(d–f) show representative MD snapshots for the strain applied along the x -direction (ϵ_x) and y -direction (ϵ_y) for the qTPC₆₀ monolayer. Fig. 7(a) and 7(d) depict the monolayer configurations at $\epsilon_x = 0$ and $\epsilon_y = 0$, respectively. We can note that the equilibrated qTPC₆₀ monolayer is not planar. It preserves its topology as the strain increase up to $\epsilon_x = 12.4\%$ (Fig. 6(b)) and to $\epsilon_x = 11.2\%$ (see Fig. 6(e)). Immediately after these critical strain values, the lattice breaks linearly with a fast crack propagation along the opposite direction of the stretch for $\epsilon_x = 12.5\%$ (Fig. 6(c)) and $\epsilon_y = 11.3\%$ (Fig. 6(f)). The same abrupt fracture mechanism occurs when the qTPC₆₀ is stretched along the x and y directions. Since the central C₆₀ unit in qTPC₆₀ is connected only with parallel covalent bonds to its next-neighboring units, the fracture pattern is the same regardless of the crystal direction.

4. Conclusions

In summary, We have carried out fully-atomistic reactive (ReaxFF) MD simulations to investigate the thermodynamic stability and stress resilience of qHPC₆₀ and qTPC₆₀, which were synthesized very recently [16]. These structures are 2D carbon-based materials composed of closely packed quasi-hexagonal and quasi-tetragonal crystalline phases of C₆₀ molecules. Their melting processes were investigated by employing heating ramp simulations, with temperatures varying from 300 K to 10,000 K during one ns. qHPC₆₀ and qTPC₆₀ maintain their structural integrity up to 3500 K. After this critical value, the thermal vibrations impose substantial changes in their morphologies, and the melting process occurs. We obtained similar melting points of 3898 K and 3965 K for qHPC₆₀ and qTPC₆₀, respectively. The melting process of these structures occurs differently. For the qHPC₆₀, the C₆₀ units are fragmented into several linear atomic chains (LACs) at 1600 K. The qTPC₆₀ structure, in turn, tends to fragment into separated C₆₀ units at 1200 K. For the stress response as a function of the uniaxial applied strain, the first noticeable feature is that qHPC₆₀ and qTPC₆₀ have a anisotropic mechanical behavior. They are more resilient to tension along the x -direction than along the y -one. The presence of a ring composed of four carbon atoms linking the C₆₀ units makes them less resilient to tension along the y -direction. Moreover, these materials present a well-defined (linear) elastic region when subjected to uniaxial tensile loading. qHPC₆₀ and qTPC₆₀ undergo an abrupt structural transition to a fractured form after a critical strain. qHPC₆₀ monolayer breaks abruptly with fast and linear crack propagation when stretched along the x -direction. Conversely, non-linear rapid crack propagation was observed by stretching qHPC₆₀ along the y -direction. A similar abrupt fracture mechanism occurs when the qTPC₆₀ is stretched along the x and y directions. Since a central C₆₀ unit in qTPC₆₀ is connected only with parallel covalent bonds to its next-neighboring units, the fracture pattern is the same regardless of the crystal direction.

The following Young's modulus values for qHPC₆₀ and qTPC₆₀ were estimated: 175.9 GPa (218.5 GPa) for x -direction (y -direction) and 100.7 GPa (133.5 GPa) for x -direction (y -direction), respectively. qHPC₆₀ tends to be more resilient than qTPC₆₀ due to the higher number of covalent bonds connecting the next-neighboring C₆₀ units.

CRediT authorship contribution statement

L.A. Ribeiro Junior: Data curation, Formal analysis, Methodology, Writing – original draft. **M.L. Pereira Junior:** Data curation, Formal analysis, Methodology, Writing – original draft. **W.F. Giozza:** Conceptualization, Supervision, Funding acquisition, Writing – review & editing. **R.M. Tromer:** Data curation, Formal analysis, Methodology, Writing – original draft. **Douglas S. Galvão:** Conceptualization, Supervision, Funding acquisition, Writing – review & editing.

Declaration of competing interest

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: Luiz A. Ribeiro Junior reports financial support was provided by Foundation for Research Support of the Federal District. Douglas S. Galvão reports financial support was provided by State of Sao Paulo Research Foundation. Raphael M. Tromer reports financial support was provided by State of Sao Paulo Research Foundation. Luiz A. Ribeiro Junior reports financial support was provided by National Council for Scientific and Technological Development.

Data availability

No data was used for the research described in the article.

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